

RADIATION OF AN INFINITE ISOTHERMAL CYLINDER  
WITH ACCOUNT OF SCATTERING

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The radiation problem of a cylinder filled by a radiating, absorbing, and scattering medium is treated. The transport equation is solved analytically within the  $P_1$  approximation for an arbitrary scattering indicatrix by the spherical harmonic method.

The transport equation of radiant energy is written for gray emission in the form [1]

$$s\nabla J + kJ = (\beta/4\pi) \int_{4\pi} P(s; s') J(r; s) d\omega' + j. \quad (1)$$

Case and Zweifel [1] obtained equations in the  $P_1$  approximation by the spherical harmonic method,

$$\nabla\psi_0 + (k - \bar{\mu}\beta)\psi_1 = \frac{3}{4\pi} \int_{4\pi} sj d\omega, \quad (2)$$

$$\text{div}\psi_1 + 3\alpha\psi_0 = \frac{3}{4\pi} \int_{4\pi} jd\omega, \quad (3)$$

where  $\bar{\mu} = \frac{1}{4\pi} \int_{4\pi} (s; s') P(s; s') d\omega'$  is the average scattering cosine.

The quantity  $\psi_0$  is proportional to the bulk density of radiant energy, and  $\psi_1$  is proportional to the radiation flux density. For isotropic internal source functions and a constant density of the attenuated material the equation for  $\psi_0$  is

$$\nabla^2\psi_0 - 3k^2(1 - \gamma)(1 - \bar{\mu})\psi_0 = -k(1 - \bar{\mu})j_0, \quad (4)$$

where

$$j_0 = \frac{3}{4\pi} \int_{4\pi} jd\omega = 3\alpha \frac{\sigma_0 T^4}{\pi}.$$

For a cylinder with axial symmetry, Eq. (4) becomes

$$\frac{d^2\psi_0}{dr^2} + \frac{1}{r} \frac{d\psi_0}{dr} - 3k^2(1 - \gamma)(1 - \bar{\mu})\psi_0 = -k(1 - \bar{\mu})j_0. \quad (5)$$

Introducing the optical width  $\tau = \int_0^r kdr$ , we rewrite (5) in the form

$$\frac{d^2\psi_0}{d\tau^2} + \frac{1}{\tau} \frac{d\psi_0}{d\tau} - \frac{\kappa^2}{k^2} \psi_0 = \frac{1 - \bar{\mu}}{k} j_0, \quad (6)$$

where  $\kappa^2 = 3k^2(1 - \gamma)(1 - \bar{\mu})$ .

The cylinder walls are assumed to be cold and black. The Marshak boundary conditions are then

$$\int_{-1}^0 [\psi_0(\tau_0) + \mu_1\psi_1(\tau_0)] \mu d\mu = \psi_0(\tau_0) - \frac{2}{3} \psi_1(\tau_0) = 0. \quad (7)$$

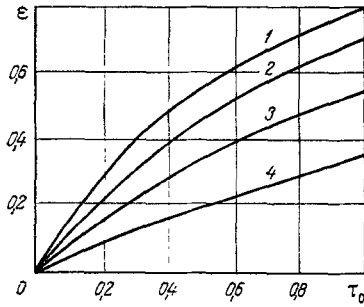


Fig. 1. Emissivities of an isothermal cylinder for  $\bar{\mu}=0.5$  and various  $\gamma$ : 1)  $\gamma=0.2$ ; 2) 0.4; 3) 0.6; 4) 0.8.

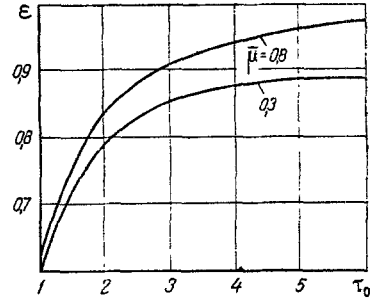


Fig. 2. Effect of average scattering cosine  $\bar{\mu}$  on emissivity.

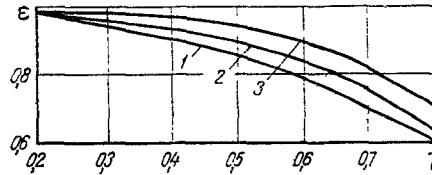


Fig. 3. Effect of  $\gamma$  on emissivity for various  $\bar{\mu}$  and  $\tau_0=4$ : 1)  $\bar{\mu}=0.2$ ; 2) 0.4; 3) 0.8.

TABLE 1. Emissivity of an Infinite Cylinder

$\tau_0$	$\epsilon$	
	by Nusselt	by Eq. (12)
0.1	0.1767	0.179
0.2	0.3170	0.328
0.4	0.5200	0.546
1.0	0.8142	0.854

The following symmetry conditions are assigned on the cylinder axis:

$$\frac{d\psi_0}{d\tau} = 0; \quad \psi_1 = 0 \quad \text{at} \quad \tau = 0. \quad (8)$$

Equation (6) is the modified Bessel equation. Its general solution is

$$\psi_0 - (1 - \gamma\bar{\mu}) i_0 \frac{k}{\kappa^2} = A I_0 \left( \frac{\kappa}{k} \tau \right) + B K_0 \left( \frac{\kappa}{k} \tau \right), \quad (9)$$

where  $I_0$  is the zero-order Bessel function of a pure imaginary argument, and  $K_0$  is the zero-order Bessel function of the first kind of a pure imaginary argument.

Since  $\psi_0$  cannot be infinite at  $\tau = 0$ , the coefficient B in (9) must be set equal to zero.

Determining A from the Marshak boundary conditions (7), we obtain

$$\psi_0(\tau) - \frac{\sigma_0 T^4}{\pi} = \left[ \frac{2}{3} \psi_1(\tau_0) - \frac{\sigma_0 T^4}{\pi} \right] \frac{I_0 \left( \frac{\kappa}{k} \tau \right)}{I_0 \left( \frac{\kappa}{k} \tau_0 \right)}, \quad (10)$$

while the quantity  $\psi_1$  at the boundary  $\tau = \tau_0$  acquires the value

$$\psi_1(\tau_0) = \frac{3\alpha \frac{1}{\kappa} \frac{\sigma_0 T^4}{\pi}}{1 + \frac{2\alpha}{\kappa} \frac{I_1(\kappa\tau_0/k)}{I_0(\kappa\tau_0/k)}} \frac{I_1 \left( \frac{\kappa}{k} \tau_0 \right)}{I_0 \left( \frac{\kappa}{k} \tau_0 \right)}. \quad (11)$$

The emissivity is determined by the expression

$$\varepsilon = 1 - \frac{1 - \frac{2\alpha}{\kappa} \frac{I_1(\kappa\tau_0/k)}{I_0(\kappa\tau_0/k)}}{1 + \frac{2\alpha}{\kappa} \frac{I_1(\kappa\tau_0/k)}{I_0(\kappa\tau_0/k)}} \quad (12)$$

The form of the scattering indicatrix is determined by the quantity  $\bar{\mu}$ . For a spherical scattering indicatrix  $P(l; l')=1$ , scattering is isotropic and  $\bar{\mu}=0$ . Cylinder emissivities were calculated by Eq. (12) for various  $\tau_0$ ,  $\gamma$ , and  $\bar{\mu}$ .

The results of these calculations are given in Figs. 1-3.

As  $\tau_0 \rightarrow \infty$ , the solution (12) transforms to the solution [2] for a semiinfinite layer:

$$\varepsilon = \frac{4\sqrt{1-\gamma}}{2\sqrt{1-\gamma} + \sqrt{3}\sqrt{1-\gamma\bar{\mu}}} \quad (13)$$

Emissivities were calculated by Eq. (12) for  $\beta=0$ . Table 1 provides the results of the calculation and a comparison with Nusselt's data as chosen from [3].

The larger the optical width of the medium and the closer to unity the ratio of the scattering coefficient to the attenuation coefficient, the more accurate the  $P_1$  approximation is.

#### NOTATION

$J$ , radiation intensity;  $r$ , radius;  $k$ , attenuation coefficient;  $\beta$ , scattering coefficient;  $\alpha$ , absorption coefficient;  $P(\mathbf{s}; \mathbf{s}')$ , scattering indicatrix;  $T$ , temperature;  $\varepsilon$ , emissivity;  $\gamma$ , scattering-to-attenuation-factor ratio.

#### LITERATURE CITED

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